



AToM

ANTENNA TOOLBOX FOR MATLAB

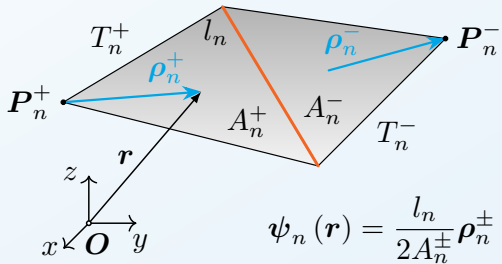
MoM-Based Matrix Operators in AToM

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Definition of RWG function.

Quadratic form of linear operator \mathcal{L} reads

$$p = \frac{1}{2} \int_{\Omega} \mathbf{J}^* \cdot \mathcal{L} \{ \mathbf{J} \} d\mathbf{r}, \quad \mathbf{J} = \mathbf{J}(\mathbf{r}), \mathbf{r} \in \Omega. \quad (1)$$

Complex power is defined as

$$P_{\text{rad}} + 2j\omega (W_m - W_e) = -\frac{1}{2} \int_V \mathbf{J}^* \cdot \mathbf{E} dV \quad (2)$$

Electric Field Integral Equation (EFIE) reads¹

$$\mathbf{E}(\mathbf{r}) = -jZ_0k \int_{\Omega} \left(\mathbf{1} + \frac{\nabla\nabla\cdot}{k^2} \right) \mathbf{J}(\mathbf{r}') \frac{e^{-jkR}}{4\pi R} dS, \quad (3)$$

with $\mathbf{1}$ being the identity matrix, $\mathbf{1} = [\delta_{pq}]$.

¹J. L. Volakis and K. Sertel, *Integral equation methods for electromagnetics*. Scitech Publishing Inc., 2012.

Usage of (finite) discretization of the source region Ω leads to

$$\mathbf{J}(\mathbf{r}) \approx \sum_{n=1}^N I_n \boldsymbol{\psi}_n(\mathbf{r}), \quad (4)$$

where $\mathbf{I} = [I_n] \in \mathbb{C}^{N \times 1}$ are expansion coefficients, $\boldsymbol{\psi}_n$ are the basis functions.

Formula (4) transforms (1) into algebraic relation

$$p \approx \frac{1}{2} \mathbf{I}^H \mathbf{L} \mathbf{I} \quad \text{with} \quad L_{mn} \equiv \int_{\Omega} \boldsymbol{\psi}_m \cdot \mathcal{L} \{ \boldsymbol{\psi}_n \} d\mathbf{r}. \quad (5)$$

Complex power (2) is approximated as

$$P_{\text{rad}} + 2j\omega (W_m - W_e) \approx \frac{1}{2} \mathbf{I}^H \mathbf{Z} \mathbf{I}, \quad (6)$$

where $\mathbf{Z} \in \mathbb{C}^{N \times N}$ is the impedance matrix defined as follows.

The impedance matrix is constructed (from normalized data) as

$$\mathbf{Z} = \mathbf{R} + j\mathbf{X} = jZ_0 a^2 \left(ka (\mathbf{Z}^{M,k} + \mathbf{Z}^{M,0}) - \frac{1}{ka} (\mathbf{Z}^{E,k} + \mathbf{Z}^{E,0}) \right), \quad (7)$$

where individual elements of the defining matrices are

$$Z_{mn}^{M,k} = \frac{1}{a^3} \int_{\Omega} \int_{\Omega} \boldsymbol{\psi}_m(\mathbf{r}) \cdot \boldsymbol{\psi}_n(\mathbf{r}') \frac{e^{-jkR} - 1}{4\pi R} dS dS', \quad (8)$$

$$Z_{mn}^{M,0} = \frac{1}{a^3} \int_{\Omega} \int_{\Omega} \boldsymbol{\psi}_m(\mathbf{r}) \cdot \boldsymbol{\psi}_n(\mathbf{r}') \frac{1}{4\pi R} dS dS', \quad (9)$$

$$Z_{mn}^{E,k} = \frac{1}{a} \int_{\Omega} \int_{\Omega} \nabla \cdot \boldsymbol{\psi}_m(\mathbf{r}) \nabla' \cdot \boldsymbol{\psi}_n(\mathbf{r}') \frac{e^{-jkR} - 1}{4\pi R} dS dS', \quad (10)$$

$$Z_{mn}^{E,0} = \frac{1}{a} \int_{\Omega} \int_{\Omega} \nabla \cdot \boldsymbol{\psi}_m(\mathbf{r}) \nabla' \cdot \boldsymbol{\psi}_n(\mathbf{r}') \frac{1}{4\pi R} dS dS'. \quad (11)$$

Normalization of characteristic modes² to unitary radiated power reads

$$\frac{1}{2} \int_{\Omega} \mathbf{J}_p^* \mathcal{Z} \{ \mathbf{J}_q \} d\mathbf{r} = (1 + j\lambda_p) \delta_{pq}. \quad (12)$$

The same normalization based on impedance matrix is³

$$\frac{1}{2} \mathbf{I}_p^H \mathbf{Z} \mathbf{I}_q = (1 + j\lambda_p) \delta_{pq}. \quad (13)$$

Physical units of impedance matrix \mathbf{Z} are $[\Omega \text{ m}^2]$.

Matrices $\mathbf{Z}^{M,k}$, $\mathbf{Z}^{M,0}$, $\mathbf{Z}^{E,k}$, $\mathbf{Z}^{E,0}$ are made dimensionless.

²M. Capek, P. Hazdra, M. Masek, *et al.*, “Analytical representation of characteristic modes decomposition,” *IEEE Trans. Antennas Propag.*, vol. 65, no. 2, pp. 713–720, 2017. DOI: 10.1109/TAP.2016.2632725.

³Complex and Hermitian conjugate can be removed in case as the characteristic modes for PEC bodies are by definition real-valued.

The analytical differentiation of \mathbf{Z} with respect to ω (normalized by ω) is

$$\omega \frac{\partial \mathbf{Z}}{\partial \omega} = jZ_0 a^2 \left(ka (\mathbf{Z}^{M,k} + \mathbf{Z}^{M,0} - jka \mathbf{T}^M) + \frac{1}{ka} (\mathbf{Z}^{E,k} + \mathbf{Z}^{E,0} + jka \mathbf{T}^E) \right), \quad (14)$$

where individual elements of the defining matrices are

$$T_{mn}^M = \frac{1}{a^4} \int_{\Omega} \int_{\Omega} \boldsymbol{\psi}_m(\mathbf{r}) \cdot \boldsymbol{\psi}_n(\mathbf{r}') \frac{e^{-jkR}}{4\pi} dS dS', \quad (15)$$

$$T_{mn}^E = \frac{1}{a^2} \int_{\Omega} \int_{\Omega} \nabla \cdot \boldsymbol{\psi}_m(\mathbf{r}) \nabla' \cdot \boldsymbol{\psi}_n(\mathbf{r}') \frac{e^{-jkR}}{4\pi} dS dS', \quad (16)$$

and

$$R = |\mathbf{r} - \mathbf{r}'|, \quad a = \max_{\mathbf{r}, \mathbf{r}' \in \Omega} \left\{ \frac{R}{2} \right\}, \quad Z_0 = \sqrt{\frac{\mu_0}{\varepsilon_0}}. \quad (17)$$

The stored energy matrix⁴ for $ka < 1$ is defined as

$$\mathbf{W} = \text{Im} \left\{ \omega \frac{\partial \mathbf{Z}}{\partial \omega} \right\}. \quad (18)$$

and the stored electric and magnetic energies are

$$\mathbf{X}_m = \frac{1}{2} (\mathbf{W} + \mathbf{X}), \quad (19)$$

$$\mathbf{X}_e = \frac{1}{2} (\mathbf{W} - \mathbf{X}). \quad (20)$$

Therefore, the following identities holds

$$\mathbf{X} = \mathbf{X}_m - \mathbf{X}_e, \quad (21)$$

$$\mathbf{W} = \mathbf{X}_m + \mathbf{X}_e. \quad (22)$$

⁴R. F. Harrington and J. R. Mautz, "Control of radar scattering by reactive loading," *IEEE Trans. Antennas Propag.*, vol. 20, no. 4, pp. 446–454, 1972. DOI: 10.1109/TAP.1972.1140234.

The basis-function overlap matrix $\Psi = [\Psi_{mn}]$ is defined as⁵ sparse matrix

$$\Psi_{mn} = \int_{\Omega} \boldsymbol{\psi}_m(\mathbf{r}) \cdot \boldsymbol{\psi}_n(\mathbf{r}) \, dS. \quad (23)$$

Properties:

- ▶ all eigenvalues are strictly positive (non-negative),
- ▶ it is a Gram matrix,
- ▶ it is sparse; sparsity for a sphere of T triangles with $N = 3T/2$ RWG basis functions is equal⁶ to $1 - 5/N$.

⁵L. Jelinek and M. Capek, “Optimal currents on arbitrarily shaped surfaces,” *IEEE Trans. Antennas Propag.*, vol. 65, no. 1, pp. 329–341, 2017. DOI: 10.1109/TAP.2016.2624735.

⁶Topologically minimal S^2 sphere is a 3-simplex (tetrahedron), then $N = 6$ and each basis function $\boldsymbol{\psi}_n$ sees all the others except of one. All opened and simple structures have higher sparsity.

The dissipation (ohmic) losses matrix $\mathbf{R}_\Omega = [R_{\Omega,mn}] \in \mathbb{R}^{N \times N}$ as

$$R_{\Omega,mn} = \int_{\Omega} R_s(\mathbf{r}) \boldsymbol{\psi}_m(\mathbf{r}) \cdot \boldsymbol{\psi}_n(\mathbf{r}) \, dS, \quad (24)$$

with $R_s(\mathbf{r}) \geq 0$ being spatially dependent surface resistivity. For $R_s(\mathbf{r}) = R_s$

$$\mathbf{R}_\Omega = R_s \boldsymbol{\Psi} \quad (25)$$

and inheriting all properties of matrix $\boldsymbol{\Psi}$.

The topological adjacency matrix $\mathbf{A} = [A_{mn}]$ can then be defined as

$$A_{mn} = \begin{cases} 1 & \Leftrightarrow \Psi_{mn} \neq 0, \\ 0 & \Leftrightarrow \Psi_{mn} = 0. \end{cases} \quad (26)$$

The dissipation loss matrix \mathbf{R}_Ω and matrix of lumped elements $\mathbf{Z}_L = [Z_{L,mn}]$ can be added to the impedance matrix as

$$\hat{\mathbf{Z}} = \hat{\mathbf{R}} + j\hat{\mathbf{X}} = \mathbf{R}_\Omega + \mathbf{Z}_L + \mathbf{Z}. \quad (27)$$

The lumped element matrix elements read

$$Z_{L,nn} = l_n^2 \left(R_n + j \left(\omega L_n - \frac{1}{\omega C_n} \right) \right). \quad (28)$$

The far-field is defined as

$$F(\hat{\mathbf{r}}, \hat{\mathbf{e}}) = \lim_{r \rightarrow \infty} \{ r e^{jk r} \hat{\mathbf{e}} \cdot \mathbf{E}(\mathbf{r}) \}. \quad (29)$$

Explicitly,

$$F(\hat{\mathbf{r}}, \hat{\mathbf{e}}) = -\frac{j Z_0 k}{4\pi} \int_{\Omega} \hat{\mathbf{e}} \cdot \mathbf{J}(\mathbf{r}') e^{jk \hat{\mathbf{r}} \cdot \mathbf{r}'} dS, \quad (30)$$

and

$$U(\hat{\mathbf{r}}, \hat{\mathbf{e}}) = \frac{1}{2Z_0} |F(\hat{\mathbf{r}}, \hat{\mathbf{e}})|^2, \quad U(\hat{\mathbf{r}}) = U(\hat{\mathbf{r}}, \hat{\boldsymbol{\varphi}}) + U(\hat{\mathbf{r}}, \hat{\boldsymbol{\psi}}), \quad (31)$$

$$P_{\text{rad}} = \int_{S^2} U(\hat{\mathbf{r}}) dS, \quad D(\hat{\mathbf{r}}, \hat{\mathbf{e}}) = \frac{4\pi U(\hat{\mathbf{r}}, \hat{\mathbf{e}})}{P_{\text{rad}}}. \quad (32)$$

Radiation intensity matrix $\mathbf{U} = [U_{mn}]$ for direction $\hat{\mathbf{r}}$ and polarization $\hat{\mathbf{e}}$ is defined⁷ as

$$U_{mn}(\hat{\mathbf{r}}, \hat{\mathbf{e}}) = \frac{Z_0 k^2}{32\pi^2} \int_{\Omega} \int_{\Omega} (\hat{\mathbf{e}} \cdot \boldsymbol{\psi}_m) (\hat{\mathbf{e}} \cdot \boldsymbol{\psi}_n) e^{-jk\hat{\mathbf{r}} \cdot (\mathbf{r} - \mathbf{r}')} dS dS', \quad (33)$$

and it is a rank-one matrix as the far-field vector $\mathbf{F} = [F_n]$ defined as

$$F_n(\hat{\mathbf{r}}, \hat{\mathbf{e}}) = \frac{-jZ_0 k}{4\pi} \int_{\Omega} \hat{\mathbf{e}} \cdot \boldsymbol{\psi}_n e^{jk\hat{\mathbf{r}} \cdot \mathbf{r}} dS \quad (34)$$

can be used

$$\mathbf{U}(\hat{\mathbf{r}}, \hat{\mathbf{e}}) = \frac{1}{2Z_0} \mathbf{F}^H(\hat{\mathbf{r}}, \hat{\mathbf{e}}) \mathbf{F}(\hat{\mathbf{r}}, \hat{\mathbf{e}}). \quad (35)$$

Total radiation intensity can be calculated as

$$\mathbf{U}(\hat{\mathbf{r}}) = \mathbf{U}(\hat{\mathbf{r}}, \hat{\boldsymbol{\varphi}}) + \mathbf{U}(\hat{\mathbf{r}}, \hat{\boldsymbol{\psi}}). \quad (36)$$

⁷L. Jelinek and M. Capek, "Optimal currents on arbitrarily shaped surfaces," *IEEE Trans. Antennas Propag.*, vol. 65, no. 1, pp. 329–341, 2017. DOI: 10.1109/TAP.2016.2624735.

Spherical waves can be projected onto basis functions as⁸

$$S_{\alpha n} = k\sqrt{Z_0} \int_{\Omega} \mathbf{u}_{\alpha}^{(1)}(k\mathbf{r}) \cdot \boldsymbol{\psi}_n(\mathbf{r}) \, dS, \quad (37)$$

α is multi-index σ, m, l , and $\mathbf{u}_{\alpha}^{(1)}(k\mathbf{r})$ are the spherical modes⁹.

The relationship between resistance part of impedance matrix and spherical waves matrix

$$\mathbf{R} = \mathbf{S}^T \mathbf{S}. \quad (38)$$

⁸D. Tayli, M. Capek, L. Akrou, *et al.*, “Accurate and efficient evaluation of characteristic modes,” , 2017, submitted, arXiv:1709.09976. [Online]. Available: <https://arxiv.org/abs/1709.09976>.

⁹G. Kristensson, *Scattering of electromagnetic waves by obstacles*. Edison, NJ: SciTech Publishing, an imprint of the IET, 2016.

Matrix $\mathbf{S} \in \mathbb{R}^{N_\alpha \times N}$ is a projection matrix between RWG basis and spherical waves basis. It is low-rank matrix in α , suitable for compression techniques.

For Ω being a spherical shell, the rows of matrix \mathbf{S} contains directly the expansion coefficients of corresponding spherical waves, \mathbf{I}_α , since

$$\mathbf{I}_{\alpha p}^H \mathbf{S}^T \mathbf{S} \mathbf{I}_{\alpha q} = K_\alpha \delta_{pq}, \quad (39)$$

where K_α is arbitrary constant depending on scaling.

Real part of the impedance matrix \mathbf{Z} represented in basis of spherical waves is

$$\mathbf{R}_\alpha = \mathbf{S} \mathbf{S}^T. \quad (40)$$

The radiated far-field can be expressed as

$$\mathbf{F}(\hat{\mathbf{r}}) = \frac{1}{k} \sum_{\alpha} j^{l-\tau+2} f_{\alpha} \mathbf{Y}_{\alpha}(\hat{\mathbf{r}}), \quad (41)$$

where $\mathbf{Y}_{\alpha}(\hat{\mathbf{r}})$ are the real-valued spherical vector harmonics and

$$[f_{\alpha}] = \mathbf{SI}, \quad f_{\alpha} \in \mathbb{R}^{1 \times 1}. \quad (42)$$

Then we get a series of equalities

$$P_{\text{rad}} \approx \frac{1}{2} \mathbf{I}^{\text{H}} \mathbf{R} \mathbf{I} = \frac{1}{2} |\mathbf{SI}|^2 = \frac{1}{2} \sum_{\alpha} |f_{\alpha}|^2 = \mathbf{I}^{\text{H}} \int_{S^2} \left(\mathbf{U}(\hat{\mathbf{r}}, \hat{\boldsymbol{\varphi}}) + \mathbf{U}(\hat{\mathbf{r}}, \hat{\boldsymbol{\vartheta}}) \right) dS \mathbf{I}, \quad (43)$$

with S^2 being unit sphere.

Electric and magnetic fields are approximated as

$$\mathbf{N}_{e,n}(\mathbf{r}) = -jZ_0k \int_{\Omega} \left((\hat{\mathbf{r}} \times \boldsymbol{\psi}_n) \times \hat{\mathbf{r}} + (3\hat{\mathbf{r}}(\hat{\mathbf{r}} \cdot \boldsymbol{\psi}_n) - \boldsymbol{\psi}_n) \left(\frac{1}{(kR)^2} + \frac{j}{kR} \right) \right) \frac{e^{-jkR}}{4\pi R} dS, \quad (44)$$

$$\mathbf{N}_{m,n}(\mathbf{r}) = -jk \int_{\Omega} (\hat{\mathbf{r}} \times \boldsymbol{\psi}_n) \left(1 + \frac{1}{jkR} \right) \frac{e^{-jkR}}{4\pi R} dS. \quad (45)$$

with $\mathbf{N}_e = [\mathbf{N}_{e,n}]$, $\mathbf{N}_m = [\mathbf{N}_{m,n}] \in \mathbb{C}^{N \times 3}$.

Notice then that

$$\mathbf{E}(\mathbf{r}) \approx \mathbf{N}_e(\mathbf{r}) \mathbf{I}, \quad (46)$$

$$\mathbf{H}(\mathbf{r}) \approx \mathbf{N}_m(\mathbf{r}) \mathbf{I}. \quad (47)$$

Electric dipole moment matrix $\mathbf{p} = [\mathbf{p}_n] \in \mathbb{R}^{N \times 3}$ is defined as

$$\mathbf{p}_n = \frac{j}{\omega} \int_{\Omega} \mathbf{r} \nabla \cdot \boldsymbol{\psi}_n \, dS = \frac{1}{j\omega} \int_{\Omega} \boldsymbol{\psi}_n \, dS. \quad (48)$$

Magnetic dipole moment matrix $\mathbf{m} = [\mathbf{m}_n] \in \mathbb{R}^{N \times 3}$ is defined as

$$\mathbf{m}_n = \frac{1}{2} \int_{\Omega} \mathbf{r} \times \boldsymbol{\psi}_n \, dS \quad (49)$$

Squared magnitude of the electric and magnetic dipole moments can be calculated as

$$|\mathbf{p}|^2 = \mathbf{I}^H \mathbf{P} \mathbf{I}, \quad (50)$$

$$|\mathbf{m}|^2 = \mathbf{I}^H \mathbf{M} \mathbf{I}, \quad (51)$$

where matrices $\mathbf{P} \in \mathbb{R}^{N \times N}$ and $\mathbf{M} \in \mathbb{R}^{N \times N}$ are

$$\mathbf{P} = \mathbf{p} \mathbf{p}^H, \quad (52)$$

$$\mathbf{M} = \mathbf{m} \mathbf{m}^H. \quad (53)$$

Useful relations¹⁰ are

$$\nabla \cdot \boldsymbol{\psi}_n(\mathbf{r}) = \pm \frac{l_n}{A_n^\pm}, \quad (54)$$

$$\int_{\Omega} \boldsymbol{\psi}_n(\mathbf{r}) \, dS = l_n (\mathbf{r}_n^{c+} - \mathbf{r}_n^{c-}), \quad (55)$$

$$\int_{\Omega} \mathbf{r} \times \boldsymbol{\psi}_n \, dS = \frac{l_n}{2} (\mathbf{P}_n^+ \times \mathbf{r}_n^{c+} - \mathbf{P}_n^- \times \mathbf{r}_n^{c-}), \quad (56)$$

$$\int_{\Omega} \nabla \cdot \boldsymbol{\psi}_m(\mathbf{r}) \, dS = \frac{l_n}{A_n^+} \int_{A_n^+} dS - \frac{l_n}{A_n^-} \int_{A_n^-} dS = 0, \quad (57)$$

where $\Omega = A_n^+ \cup A_n^-$.

¹⁰S. M. Rao, D. R. Wilton, and A. W. Glisson, "Electromagnetic scattering by surfaces of arbitrary shape," *IEEE Trans. Antennas Propag.*, vol. 30, no. 3, pp. 409–418, 1982. DOI: 10.1109/TAP.1982.1142818.

For $\mathbf{r} \equiv [x \ y \ z]$ the transformation from/to simplex coordinates (α, β, γ) reads

$$\mathbf{r} = [\alpha \ \beta \ \gamma] \begin{bmatrix} \mathbf{P}_A \\ \mathbf{P}_B \\ \mathbf{P}^\pm \end{bmatrix}. \quad (58)$$

Notice that $\gamma = 1 - \alpha - \beta$, and

$$\int_T f(\mathbf{r}) \, dS = 2A \int_0^1 \int_0^{1-\alpha} f(\alpha \mathbf{P}_A + \beta \mathbf{P}_B + (1 - \alpha - \beta) \mathbf{P}^\pm) \, d\beta \, d\alpha. \quad (59)$$

Discretization grid and RWG basis functions:

Listing 1: atom_code1_mesh.m

```
% Frequency
f = atom.selectedProject.physics.getFrequencyListValues;
% or manually specified by user:
f = 1e9; % 1 GHz

% (It is expected that MoM requests are correctly set up.)
Res = atom.selectedProject.solver.MoM2D.results;

Mesh = Res.mesh;          % mesh grid
BF    = Res.basisFcns;    % basis functions

% Or without running MoM solver directly from AToM:
Mesh = atom.selectedProject.mesh.getMeshData2D();
BF    = models.solvers.MoM2D.basisFcns.getBasisFcns(Mesh);
```

Impedance matrix(-related) operators \mathbf{Z} , \mathbf{W} , $\mathbf{Z}^{M,k}$, $\mathbf{Z}^{M,0}$, $\mathbf{Z}^{E,k}$, $\mathbf{Z}^{E,0}$, \mathbf{T}^M , \mathbf{T}^E :

Listing 2: atom_code1_MoM1.m

```

% Impedance matrix
Z = Res.zMat.data;

omega = 2*pi*f;
% Stored energy matrix
W = omega*imag(Res.zMatD.data); % omega*DZ!

% Individual parts of impedance matrix:
ZMk = Res.zMatMk.data;
ZM0 = Res.zMatM0.data;
ZEK = Res.zMatEk.data;
ZE0 = Res.zMatE0.data;
TE = Res.tMatE.data;
TM = Res.tMatM.data;
  
```

Alternatively, \mathbf{Z} and \mathbf{W} can be calculated directly from normalized blocks:

Listing 3: atom_code1.MoM2.m

```
% Circumscribing sphere
a = models.utilities.meshPublic.getCircumsphere(Mesh.nodes);
% Wavenumber and electrical size
k = models.utilities.converter.f0tok0(f);
ka = k*a;

% Normalization constant
C = a^2*Z0;

% Impedance matrix and stored energy matrix
Z = 1j*C*(ka*(ZMk + ZM0) - 1/ka*(ZEK + ZE0));
W = imag(1j*C*(ka*(ZMk + ZM0 - 1j*ka*TM) + 1/ka*(ZEK + ZE0 + 1j*ka*TE)));
```


Basis-function overlap matrix Ψ and related matrices \mathbf{R}_Ω and \mathbf{A} :

Listing 4: atom_code1.LossyMatrix.m

```
% The basis-function overlap matrix
Psi = models.utilities.matrixOperators.ohmicLosses.lossyMatrix(Mesh, BF);

% Dissipation losses matrix
Romega = Rs*Psi;

% RWG adjacency matrix
A = double(logical(Psi));
```

Far-field vectors \mathbf{F} and matrix \mathbf{U} :

Listing 5: atom_code1_farfield.m

```
% Theta and phi used to specify  $\widehat{\mathbf{r}}$ 
theta = pi/2; % from 0 to pi
phi   = 0;    % from 0 to 2*pi
% Component used to specify  $\widehat{\mathbf{e}}$ 
component = 'theta'; % component = {'theta' | 'phi' | 'total'}

% Far-field matrix (U) and vectors (F)
[U, F_phi, F_theta] = ...
    models.utilities.matrixOperators.farfield.computeU...
    (Mesh, BF, f, theta, phi, component)
```

Spherical wave projection matrix \mathbf{S} :

Listing 6: atom_code1_sphericalwaves.m

```
nQuad = 1; % order of quadrature rule
Lmax = 15; % highest degree of used Legendre polynomial

% Spherical wave projection matrix of size NxM
% N – number of spherical waves, M – number of RWG functions
S = models.utilities.matrixOperators.SMatrix.computeS...
    (Mesh, BF, f, Lmax, nQuad);
```

Electric and magnetic dipole matrices \mathbf{P} and \mathbf{M} , and vectors \mathbf{p} and \mathbf{m} :

Listing 7: atom_code1_elmagMoments.m

```
% Electric moment matrix (P) and vector (p)
[P, p] = models.utilities.matrixOperators.electricMoment.computeP...
    (Mesh, BF, f);

% Magnetic moment matrix (M) and vector (m)
[M, m] = models.utilities.matrixOperators.magneticMoment.computeM...
    (Mesh, BF, f);
```

Far-field approximation

$$\mathbf{E}_{\text{far}}(\mathbf{r}) = -j\omega \mathbf{A}(\mathbf{r}), \quad \mathbf{A}(\mathbf{r}) = \frac{\mu_0}{4\pi} \int_{\Omega} \mathbf{J}(\mathbf{r}') \frac{e^{-jk|\mathbf{r}-\mathbf{r}'|}}{|\mathbf{r}-\mathbf{r}'|} dS, \quad (60)$$

with amplitude $R \approx |\mathbf{r}| = r$ and phase $R \approx r - \hat{\mathbf{r}} \cdot \mathbf{r}'$ (61)

leads to

$$\mathbf{E}_{\text{far}}(\mathbf{r}) = -\frac{jZ_0k}{4\pi} \frac{e^{-jkr}}{r} \int_{\Omega} \mathbf{J}(\mathbf{r}') e^{jk\hat{\mathbf{r}} \cdot \mathbf{r}'} dS. \quad (62)$$

Questions?

For a complete PDF presentation see

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